

IN THE CLAIMS

Please amend the claims as follows:

Claim 1 (Currently Amended): An aluminum magnesium titanate honeycomb carrier for an exhaust gas-cleaning catalyst, wherein the material for the aluminum magnesium titanate honeycomb carrier is an aluminum magnesium titanate sintered product obtained by firing at from 1,000 to 1,700°C a raw mixture comprising:

100 parts by mass, as calculated as oxides, of a mixture comprising a Mg-containing compound, an Al-containing compound and a Ti-containing compound in the same metal component ratio as the metal component ratio of Mg, Al and Ti in an aluminum magnesium titanate represented by the empirical formula  $Mg_xAl_{2(1-x)}Ti_{(1+x)}O_5$  (wherein  $0 < x \leq 0.5$ ); and

from 1 to 10 parts by mass of an alkali feldspar represented by the empirical formula  $(Na_yK_{1-y})AlSi_3O_8$  (wherein  $0 < y < 1$ ); and

a remaining ratio  $[[\beta]]\alpha$  (%) of the aluminum magnesium titanate honeycomb carrier is higher than the remaining ratio  $[[\beta]]\alpha$  (%) of an aluminum titanate honeycomb carrier after both the aluminum magnesium titanate honeycomb carrier and the aluminum titanate honeycomb carrier are held at 1100 1000°C for 100 hrs, wherein the aluminum titanate honeycomb carrier is obtained by firing at 1400°C a mixture of  $\alpha$ -alumina and anatase-type titanium oxide and an alkali feldspar represented by  $(Na_{0.6}K_{0.4})AlSi_3O_8$ .

Claims 2-3 (Canceled).

Claim 4 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, having a wall thickness in a range of 0.05 to 0.6 mm, a cell density in a range of 15 to 124 cells/cm<sup>2</sup>, a porosity of the partition wall in a range of 20 to 50%, and a thermal expansion coefficient of at most  $3.0 \times 10^{-6} K^{-1}$ .

Claim 5 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, wherein the catalyst comprises an alkali metal or alkaline earth metal component to remove NOx in the exhaust gas.

Claim 6 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, wherein the exhaust gas is an exhaust gas of an automobile wherein a fuel is directly jetted into an engine, or of a system wherein a fuel is diluted and burned.

Claims 7-11 (Canceled).

Claim 12 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to claim 1, wherein the raw mixture comprises the alkali feldspar represented by the empirical formula  $(Na_yK_{1-y})AlSi_3O_8$  where y ranges from 0.15 to 0.85.

Claim 13 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to claim 1, wherein the raw mixture comprises the alkali feldspar in amounts in a range of 3 to 5 parts by mass.

Claim 14 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to claim 1, wherein the average particle size of the raw mixture is less than 10  $\mu m$ .

Claim 15 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to claim 1, wherein the average particle size of the raw mixture is in a range of 1 to 5  $\mu\text{m}$ .

Claim 16 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to claim 1, wherein the firing temperature is in a range of 1250 to 1450°C.

Claim 17 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, wherein the catalyst comprises potassium.

Claim 18 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, wherein said aluminum magnesium titanate honeycomb carrier does not show a peak of  $\text{KAlSiO}_4$  in the vicinity of  $2\theta=28^\circ$  in X-ray diffraction measurement in comparison to a honeycomb carrier of aluminum magnesium titanate without the alkali feldspar after a test is carried out, wherein the test comprises dipping the aluminum magnesium titanate honeycomb carrier in an aqueous potassium nitrate solution at a concentration of 1 mol/liter, drying and holding the aluminum magnesium titanate honeycomb carrier in a furnace maintained at a temperature of 900 °C for 100 hours.

Claim 19 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, wherein said aluminum magnesium titanate honeycomb carrier does not show a peak of  $\text{KAlSiO}_4$  in the vicinity of  $2\theta=28^\circ$  in X-ray diffraction measurement in comparison to a honeycomb carrier of aluminum magnesium titanate without the alkali feldspar after a test is carried out, wherein the test comprises dipping the aluminum magnesium titanate honeycomb carrier in an aqueous potassium nitrate solution at a

concentration of 1 mol/liter, drying and holding the aluminum magnesium titanate honeycomb carrier in a furnace maintained at a temperature of 900 °C for 150 hours.

Claim 20 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, wherein said aluminum magnesium titanate honeycomb carrier does not show a peak of  $KAlSiO_4$  in the vicinity of  $2\theta=28^\circ$  in X-ray diffraction measurement in comparison to a honeycomb carrier of aluminum magnesium titanate without the alkali feldspar after a test is carried out, wherein the test comprises dipping the aluminum magnesium titanate honeycomb carrier in an aqueous potassium nitrate solution at a concentration of 1 mol/liter, drying and holding the aluminum magnesium titanate honeycomb carrier in a furnace maintained at a temperature of 900 °C for 200 hours.

Claim 21 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, wherein the material for the aluminum magnesium titanate honeycomb carrier is an aluminum magnesium titanate sintered product obtained by firing at from 1300 to 1450°C a raw mixture comprising:

100 parts by mass, as calculated as oxides, of a mixture comprising a Mg-containing compound, an Al-containing compound and a Ti-containing compound in the same metal component ratio as the metal component ratio of Mg, Al and Ti in an aluminum magnesium titanate represented by the empirical formula  $Mg_xAl_{2(1-x)}Ti_{(1+x)}O_5$  (wherein  $0 < x < 1$ ); and

from 1 to 10 parts by mass of an alkali feldspar represented by the empirical formula  $(Na_yK_{1-y})AlSi_3O_8$  (wherein  $0 < y < 1$ ), and

a difference between a remaining ratio  $\beta$  (%) of the aluminum magnesium titanate honeycomb carrier and the remaining ratio  $\beta$  (%) of an aluminum titanate honeycomb carrier is from 4% to 16% when both the aluminum magnesium titanate honeycomb carrier and the

aluminum titanate honeycomb carrier are held at 1000°C for from 80 to 100 hrs, wherein the aluminum titanate honeycomb carrier is obtained by firing at 1400°C a mixture of  $\alpha$ -alumina and anatase-type titanium oxide and an alkali feldspar represented by  $(Na_{0.6}K_{0.4})AlSi_3O_8$ .

Claim 22 (Previously Presented): The aluminum magnesium titanate honeycomb carrier according to Claim 1, wherein a difference between a remaining ratio  $\beta$  (%) of the aluminum magnesium titanate honeycomb carrier and the remaining ratio  $\beta$  (%) of an aluminum titanate honeycomb carrier is from 4% to 16% when both the aluminum magnesium titanate honeycomb carrier and the aluminum titanate honeycomb carrier are held at 1000°C for from 80 to 100 hrs, wherein the aluminum titanate honeycomb carrier is obtained by firing at 1400°C a mixture of  $\alpha$ -alumina and anatase-type titanium oxide and an alkali feldspar represented by  $(Na_{0.6}K_{0.4})AlSi_3O_8$ .